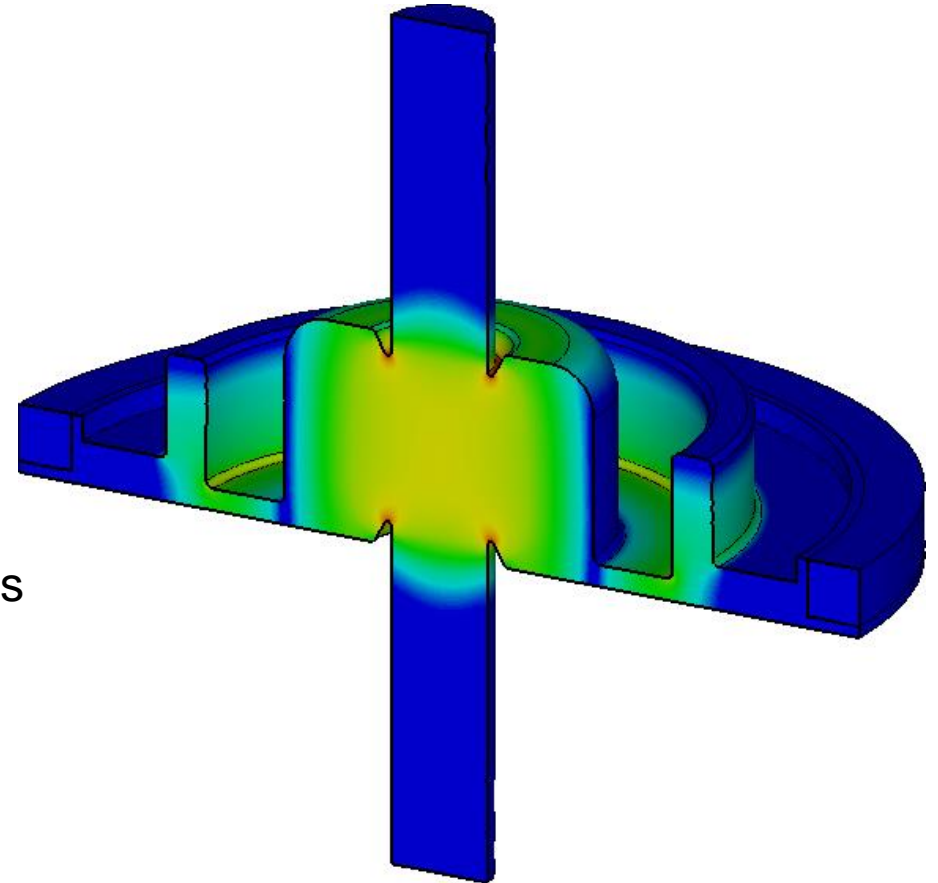


# Numerical Optimization of the Shintake Cavity

Simon Karau, Peter Hülsmann, Michael Bousonville, Silke Vilcins  
Hamburg, MHF, 2023-12-04



# Overview

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### 2. One-Cell 1.5 GHz Choke-Mode-Cavity

- General Cavity Structure and Optimization of  $TM_{010}$  Mode by CST Eigenmodesolver
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- Mode Overview of Nose-Coned Choke-Mode-Cavity by CST Eigenmodesolver

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- Specification of the Coupler & Tuner System
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## Concept of the Choke-Mode-Cavity by T. Shintake 1992

### Cylindrically Radial-Line ending with a Damper on a Cavity

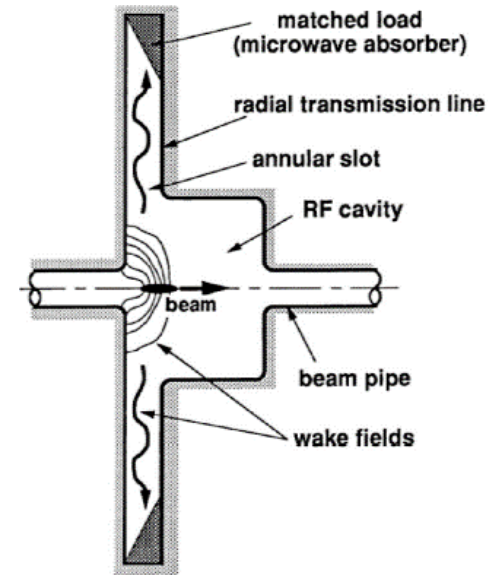
- All TM-Modes (and most TE-Modes) will excite the Radial-Line
- and will be attenuated by the Damper.

### Adding a Choke in the Radial-Line to protect $TM_{010}$ Mode

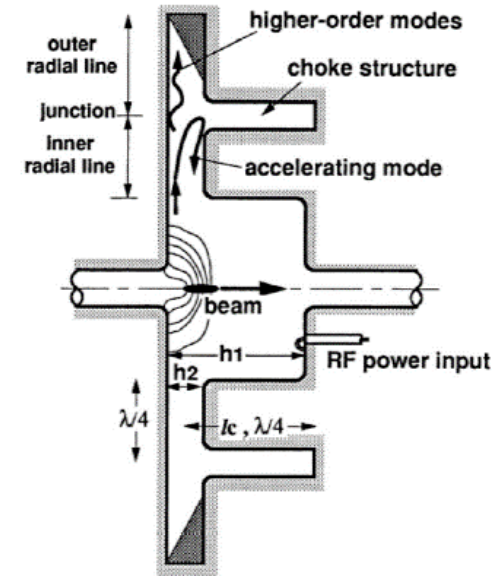
- The **Short** will be transformed by  $\lambda/4$  into an **Open**.
- Serial junction added impedance  $Z_{\text{choke}} = \infty$  and  $Z_{\text{damper}}$   
$$Z_{\text{junction}} = Z_{\text{choke}} + Z_{\text{damper}} = \infty \text{ (Open)}$$
and has a infinitely impedance independent of the damper.
- Distance of  $\lambda/4$  transforms the **Open** into a **Short** with  $Z_{\text{wall}} = 0$ .

### Damping of Higher Order Modes (HOMs):

- Almost all HOMs are strongly attenuated  
-> Only not critical  $TE_{0nq}$  can not excite the Radial-Line
- The  $TM_{010}$  acceleration Mode is protected by the Choke  
-> Only current losses will attenuate the  $TM_{010}$  Mode (perfect Choke)



(a) Radial Line Damper



(b) Choke Mode Cavity

Sketch from T. Shintake, "The Choke Mode Cavity", 1992.

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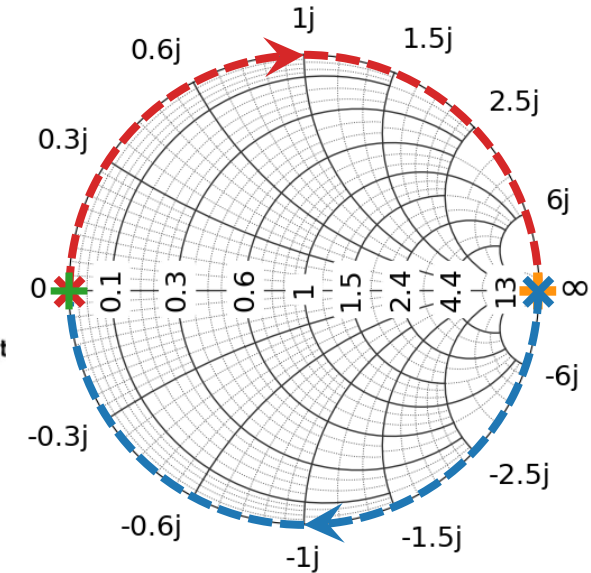
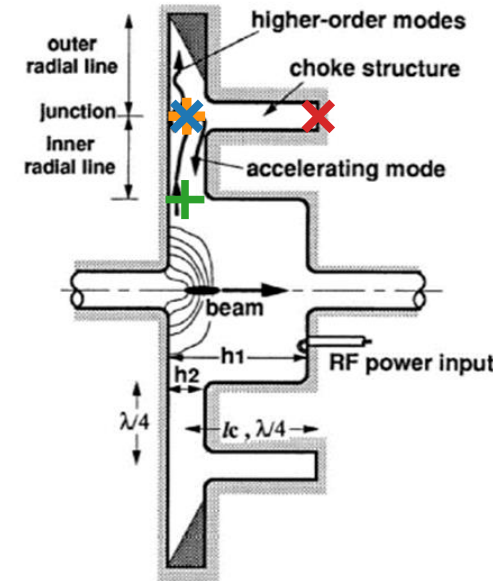
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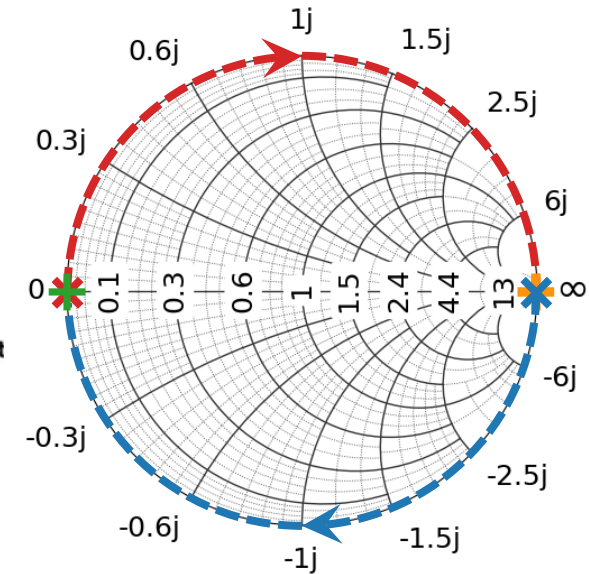
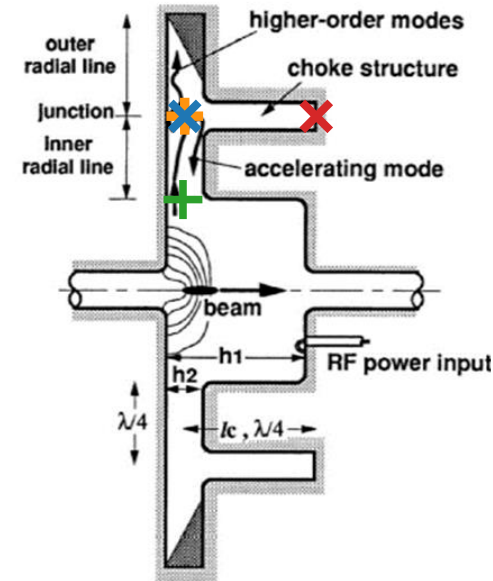
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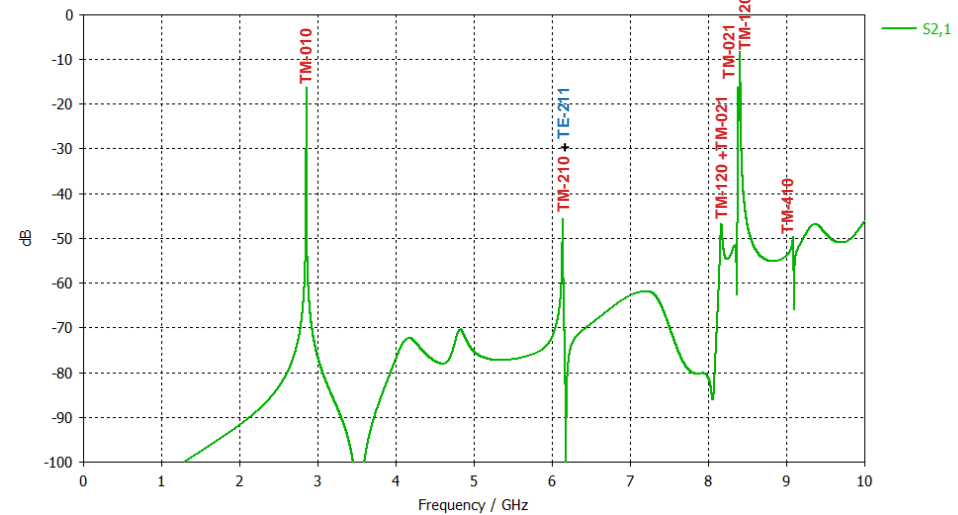
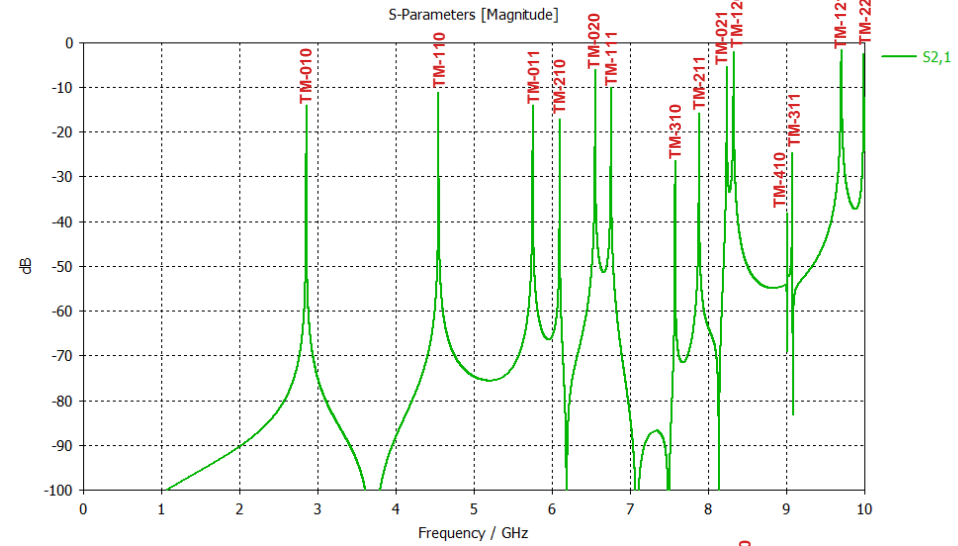
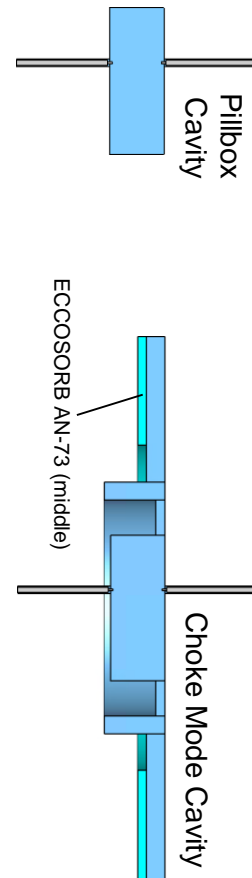
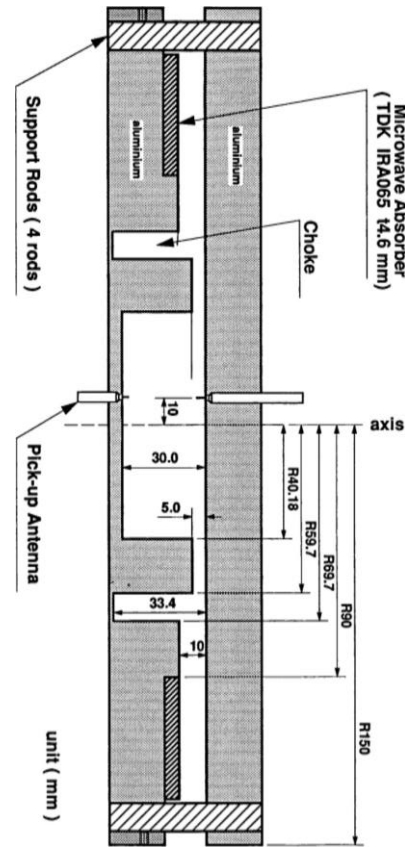
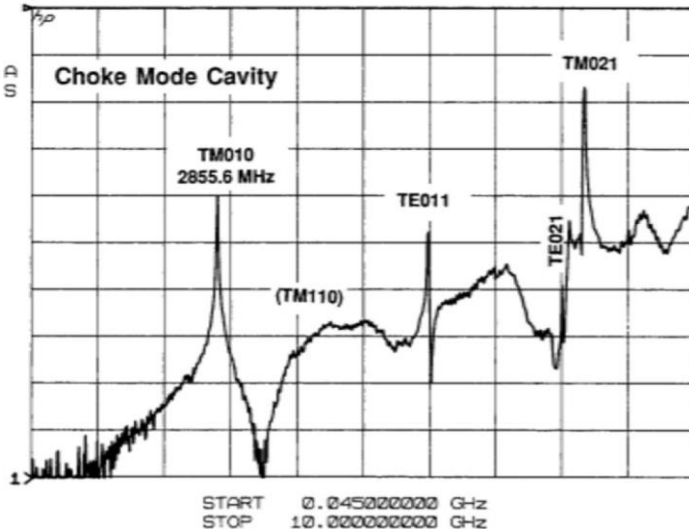
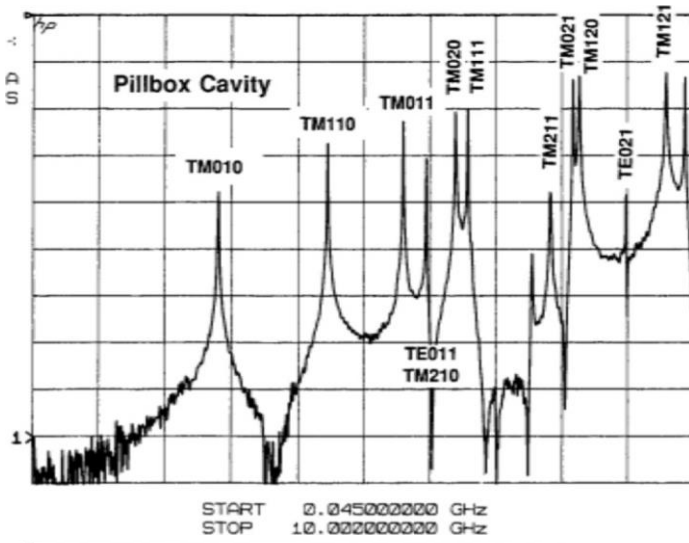
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Rough Verification of Measured Cavity Spectrum of the Original Paper by CST Frequency-Domain-Solver

Cavity S-Params. from T. Shintake, "The Choke Mode Cavity", 1992

CST Frequency-Domain-Solver S-Params.

Resonance spectrum of (a) the pillbox cavity, and (b) the choke mode cavity.  
Vertical scale: 10 dB/div, frequency scale: 1 GHz/div, frequency span: 0 to 10 GHz.



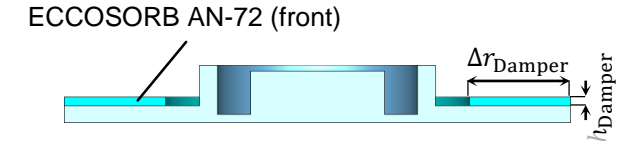
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## General Cavity Structure and Optimization of $TM_{010}$ Mode by CST Eigenmodesolver

### 1.5 GHz Pill-Box Choke-Mode-Cavity (CMC)

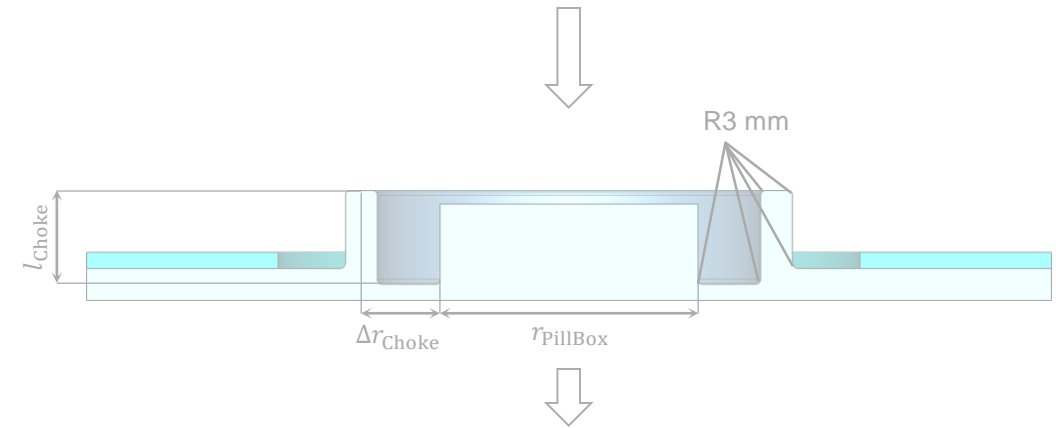
#### I. Starting Point

- Exemplary 2.867 GHz Cavity from *T. Shintake, "The Choke Mode Cavity", 1992*
- Damper:
  - CST Material Library: ECCOSORB AN-72 (front)
  - $\Delta r_{\text{Damper}} = 60 \text{ mm}$  &  $h_{\text{Damper}} = 5 \text{ mm}$



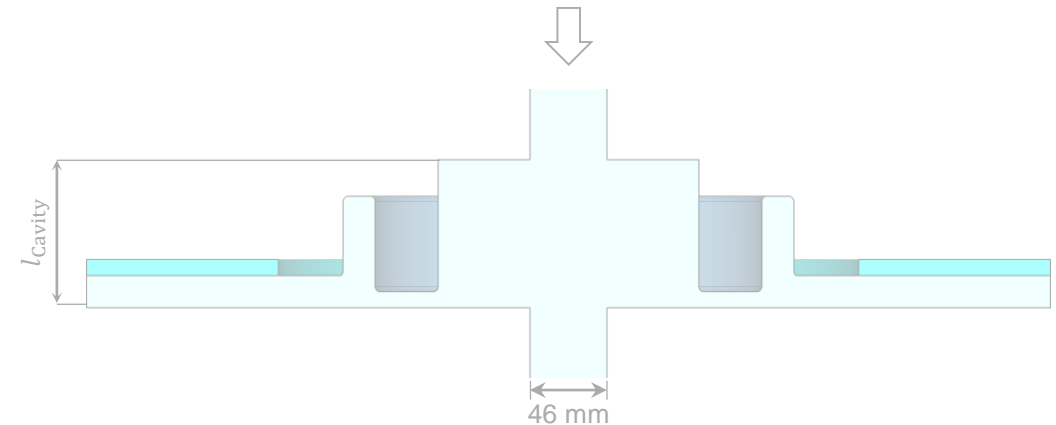
#### II. Scaling of the Model to 1.5 GHz

- Scaling by Factor 1.9 & Rounding Edges with  $R = 3 \text{ mm}$
- Reoptimization of the Structure by CST Eigenmodesolver
  - Get  $r_{\text{PillBox}}$  to get  $f_{\text{res}} = 1.500 \text{ GHz}$
  - Find  $l_{\text{Choke}}$  &  $\Delta r_{\text{Choke}}$  by Iterations for:
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#### III. Pill-Box Choke-Mode-Cavity with Beam-Pipe

- Adding the  $\varnothing = 46 \text{ mm}$  Petra IV Beam-Pipe
- Optimization of Pill-Box Length  $l_{\text{Cavity}}$  for max.  $R_{\text{sh,eff}}$
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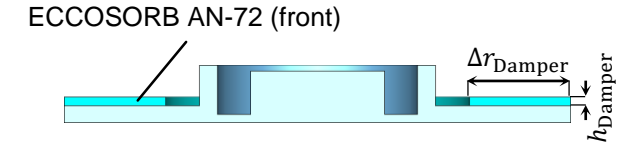
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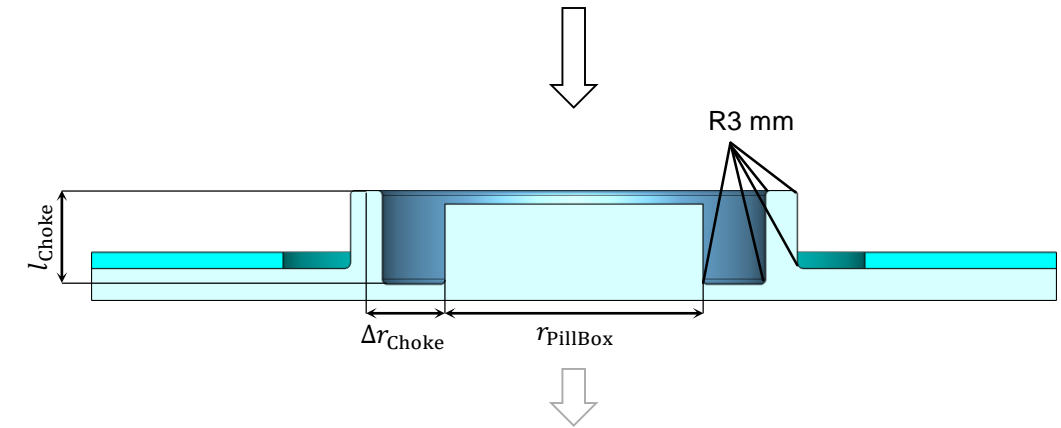
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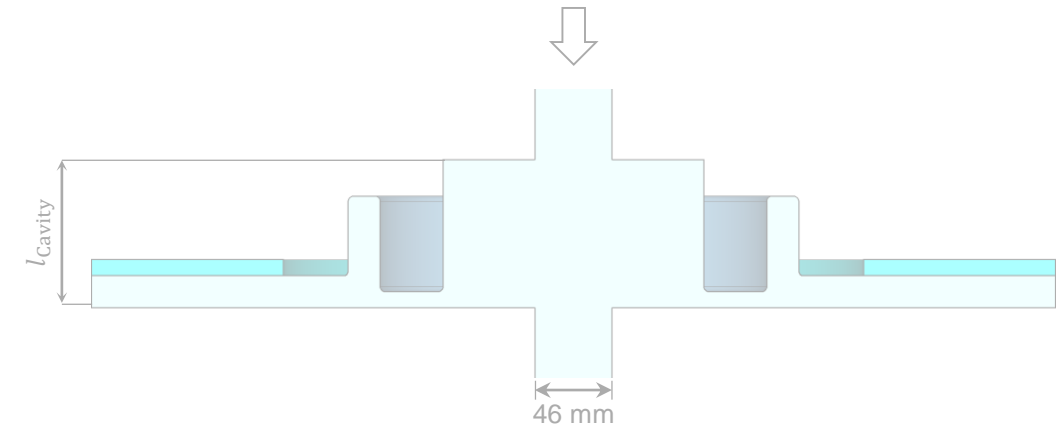
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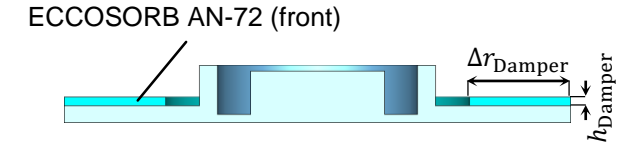
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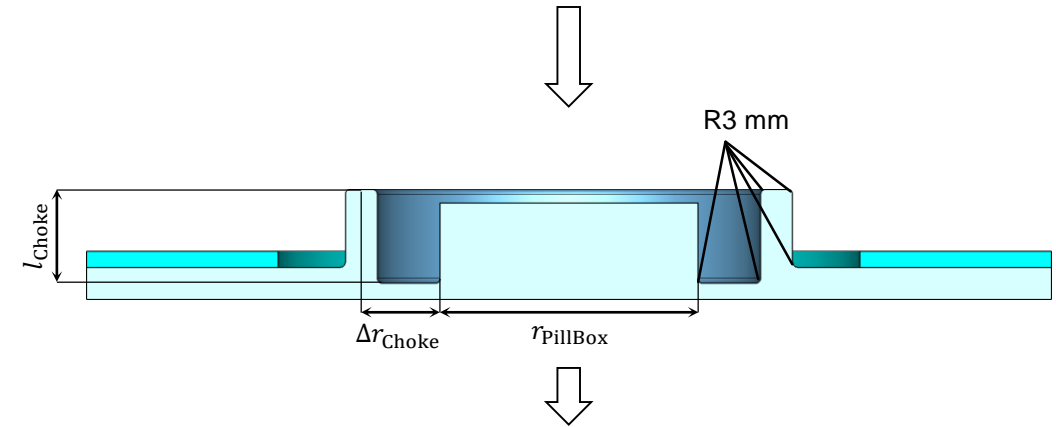
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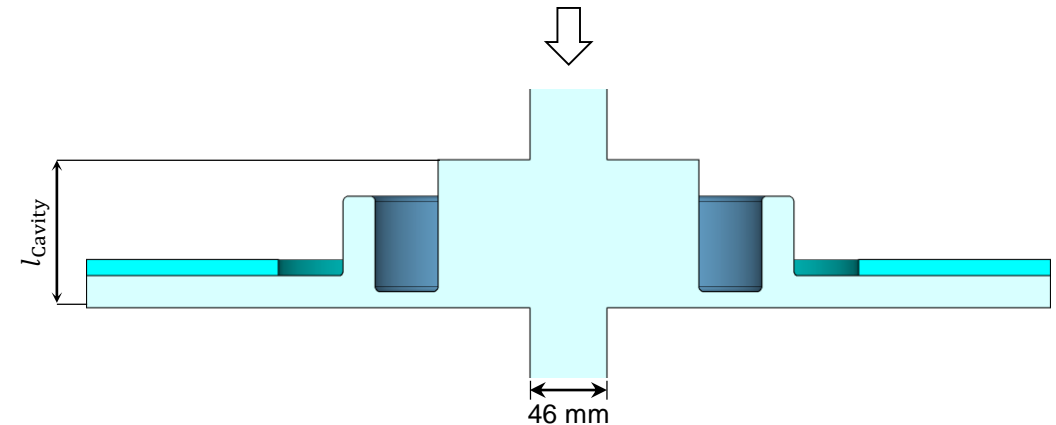
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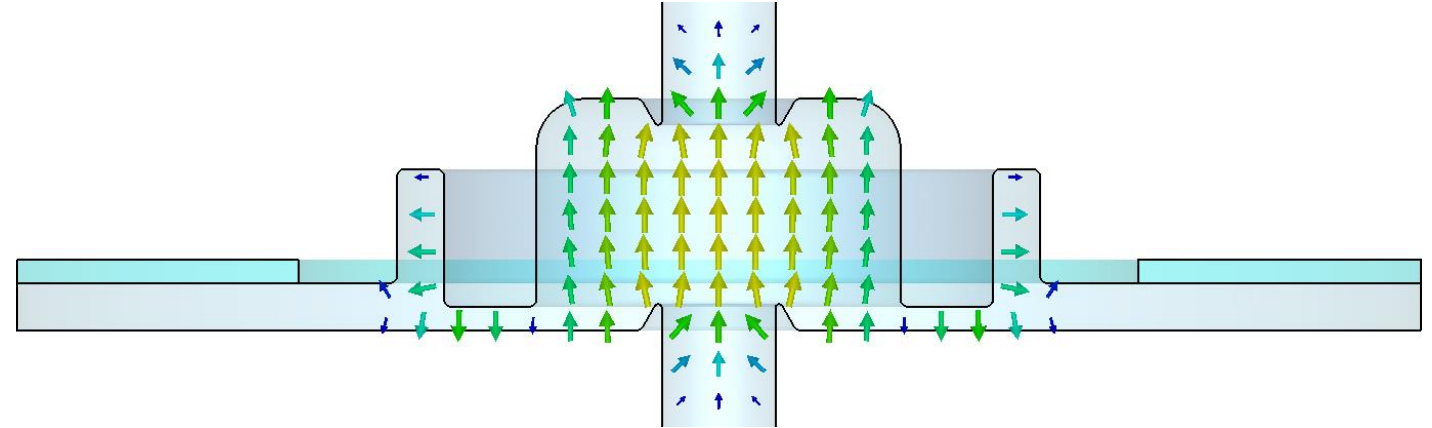
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## General Cavity Structure and Optimization of $TM_{010}$ Mode by CST Eigenmodesolver

### Nose-Cone Optimization

For further Optimization of the Cavity

- Noses are included:
  - At the Transitions of Cavity and Beam-Pipe
  - to increase the Volume of Stored Energy.
- Rounding of the outer Cavity Edges:
  - Reduces the Losses of the Cavity,
  - but are not used at the Back-Side, to ensure
  - the excitation of the Radial-Line by all TM-Modes.



|                               | Pill-Box with Beam-Pipe |                                 | Nose-Cone with Beam-Pipe |                                  |
|-------------------------------|-------------------------|---------------------------------|--------------------------|----------------------------------|
| $q_{TM_{010}}$                | Pill-Box                | Pill-Box with Choke-Mode-Damper | Nose-Cone                | Nose-Cone with Choke-Mode-Damper |
| $f_{res}$ [GHz]               | 1.500                   | 1.500                           | 1.500                    | 1.500                            |
| $Q_0$ [1]                     | 24153                   | 20492 (85%)                     | 23216                    | 19782 (85%)                      |
| $R_{sh,eff}$ [M $\Omega$ ]    | 1.899                   | 1.468 (77%)                     | 2.202                    | 1.706 (77%)                      |
| $R_{sh,eff}/Q_0$ [ $\Omega$ ] | 78.6                    | 71.6 (91%)                      | 94.8                     | 86.2 (91%)                       |
| $\Delta_c$ [1]                | 61%                     | 61%                             | 66%                      | 66%                              |

## 2. One-Cell 1.5 GHz Choke-Mode-Cavity

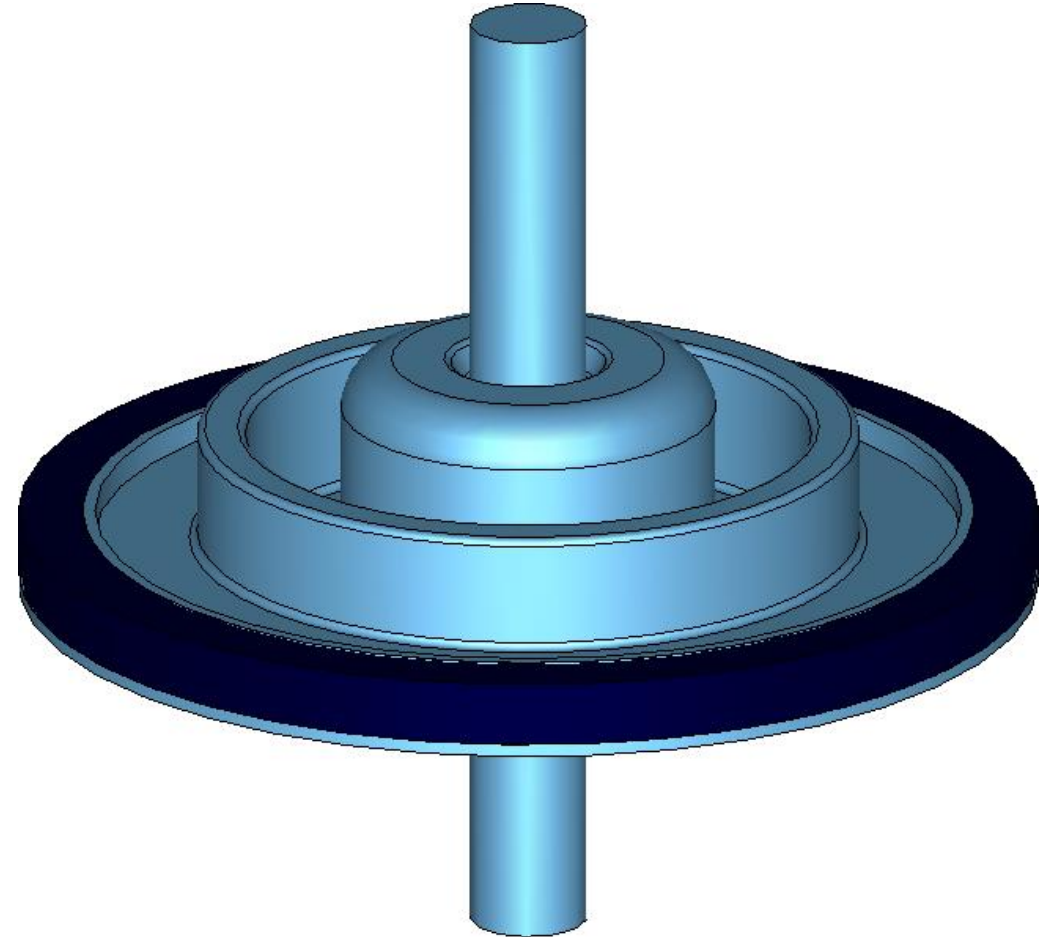
### Selection of a Damping Material

#### General selection of an Damping Material

- First Simulations used non-practical Damping Materials
  - As a real usable Damping Material
    - the Idea of single Ring of Siliziumcarbid (SiC) was adapted from
    - *T. Inagaki et al., "High-gradient C-Band Linac for a Compact X-Ray Free-Electron Laser Facility", 2014.*
- because of the simplicity and suitable Material Properties

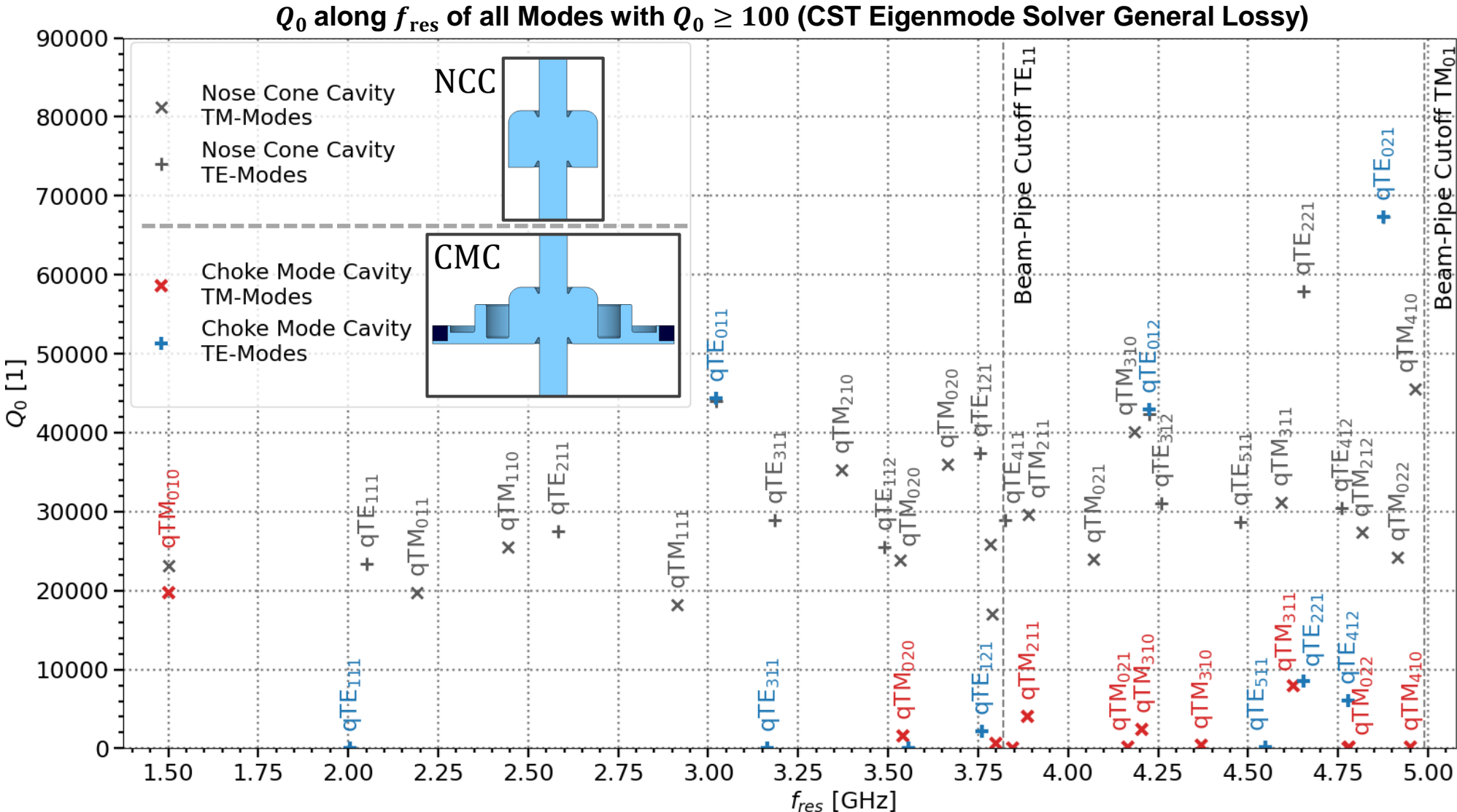
#### Simulation Parameters

- RF Material Parameters ( $\epsilon_r$ ) of SiC vary widely between
  - Manufacturing Technique,
  - Frequency and
  - Temperatureand must be measured to get precise Values.
- For Simulation before a Material Measurement
  - $\epsilon_r = 20$
  - $\tan\delta_E = 0.25$are used.



# 2. One-Cell 1.5 GHz Choke-Mode-Cavity

## Mode Overview of Nose-Coned Choke-Mode-Cavity by CST Eigenmodesolver



### Results

#### qTM<sub>010</sub> Mode

- $Q_0(\text{NCC}) = 23157$
- $Q_0(\text{CMC}) = \frac{19784}{85\%}$

#### Decreasing of other qTM

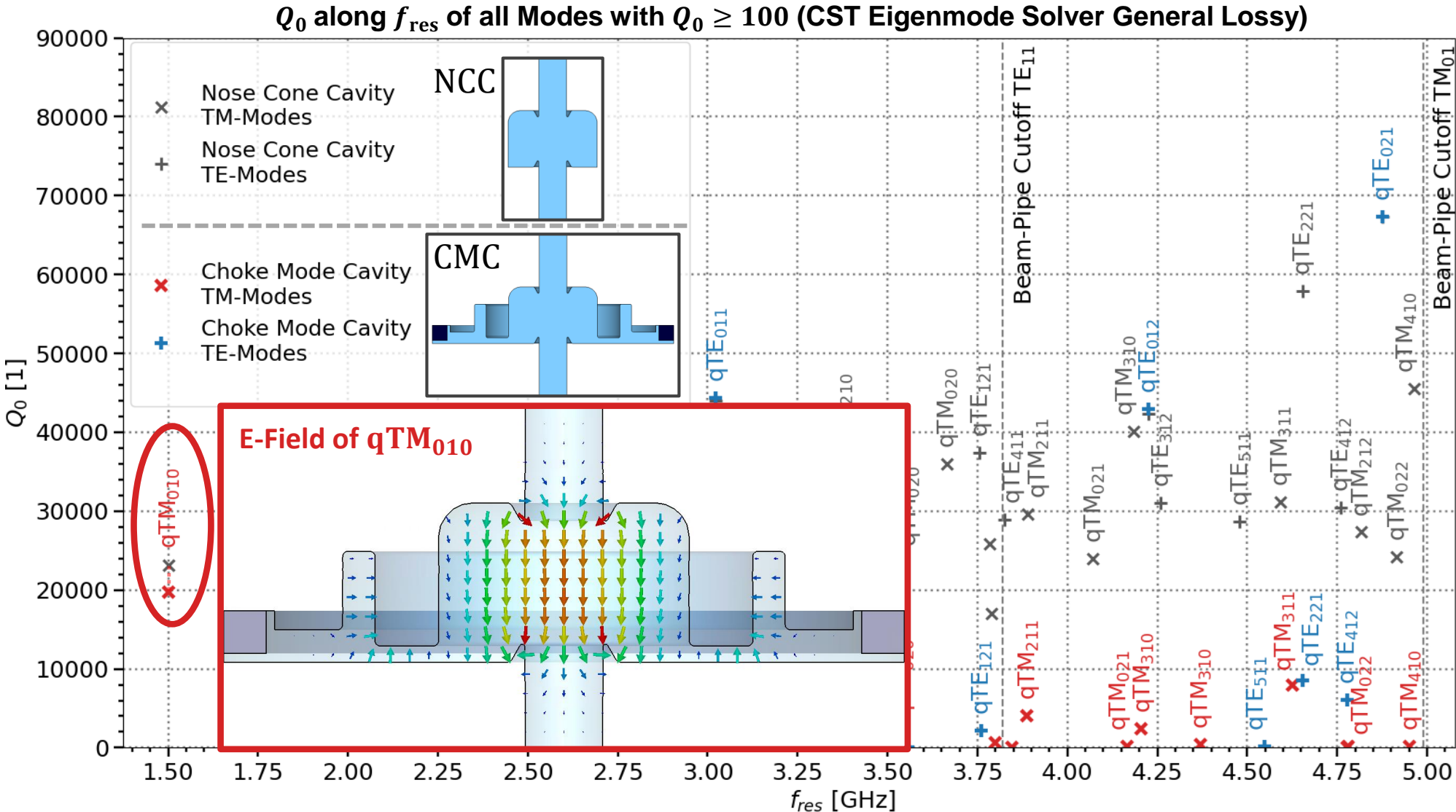
- Strongly reduced  $Q_0$ :  
 $Q_0(\text{qTM}_{011}) \approx 8$   
 $Q_0(\text{qTM}_{110}) \approx 17$
- Highest HOM-TM:  
 $Q_0(\text{qTM}_{311}) \approx 8000$   
 with  $f_{res}$  next to  
 Choke 3<sup>rd</sup> resonance  
 $4.5\text{GHz} = 3 \cdot 1.5\text{GHz}$

#### Decreasing of qTE

- Most qTE are also strongly reduced
- Only qTE<sub>0nq</sub> are undamped, because can not excite Radial-Line

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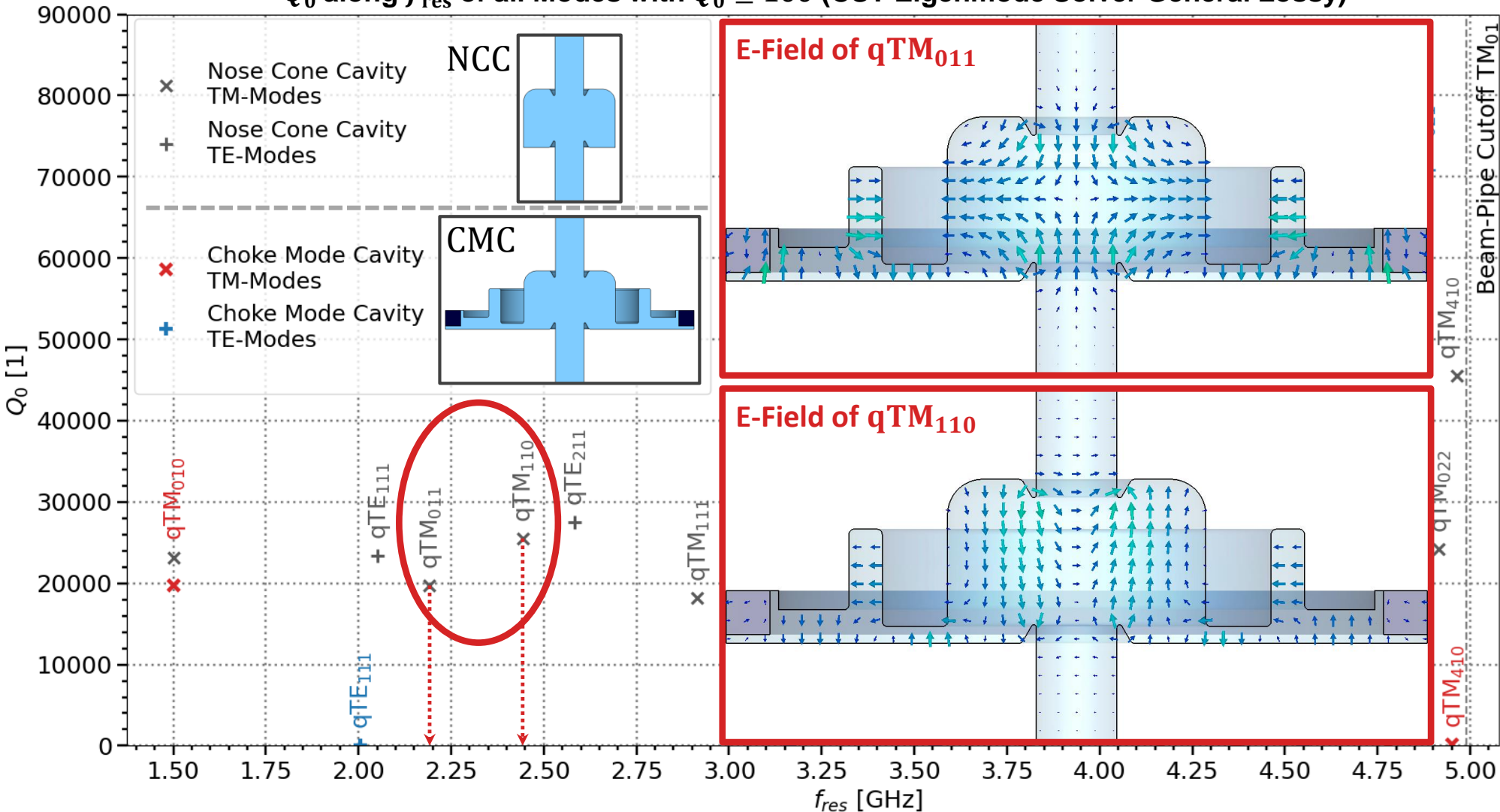
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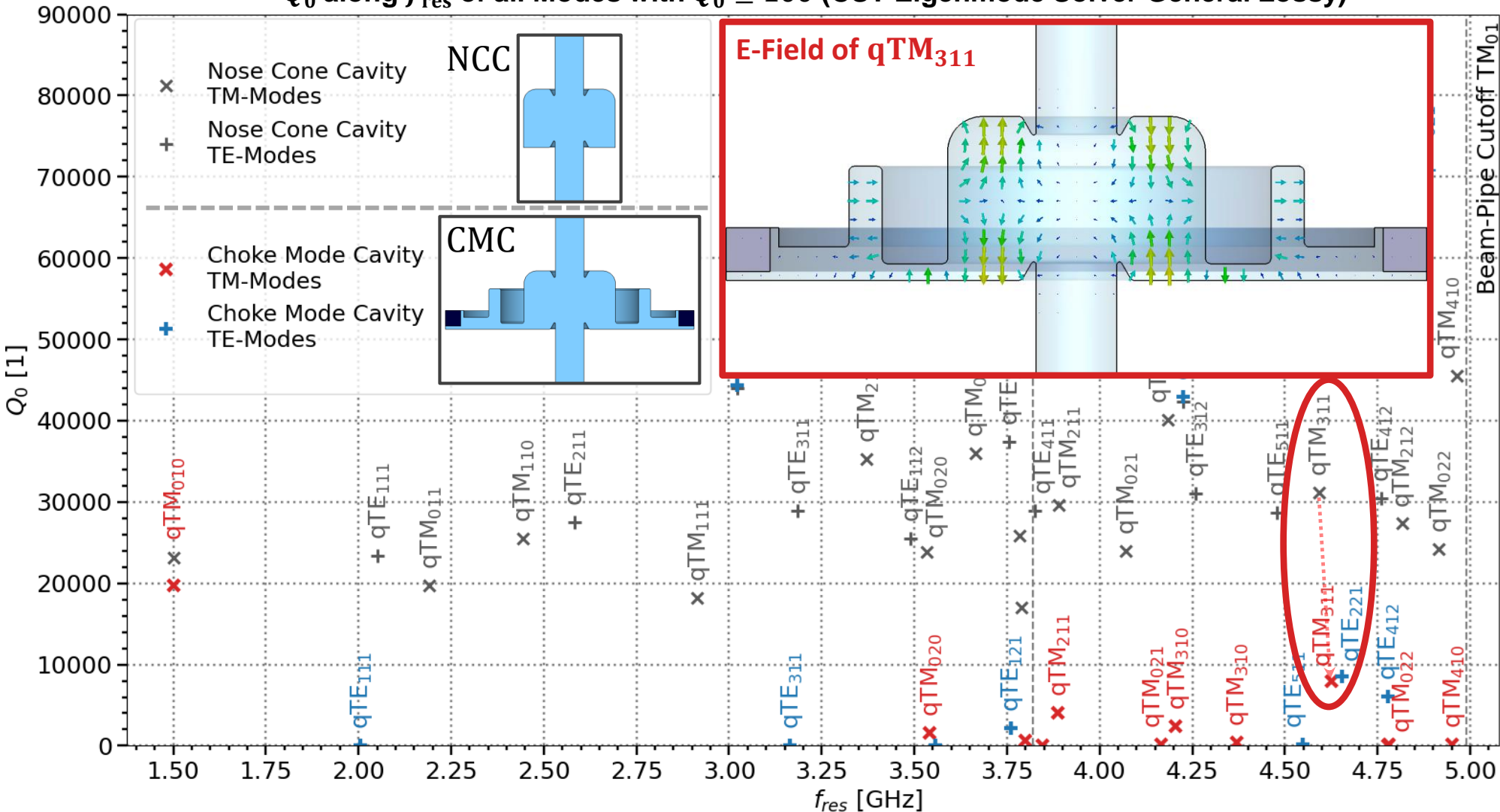
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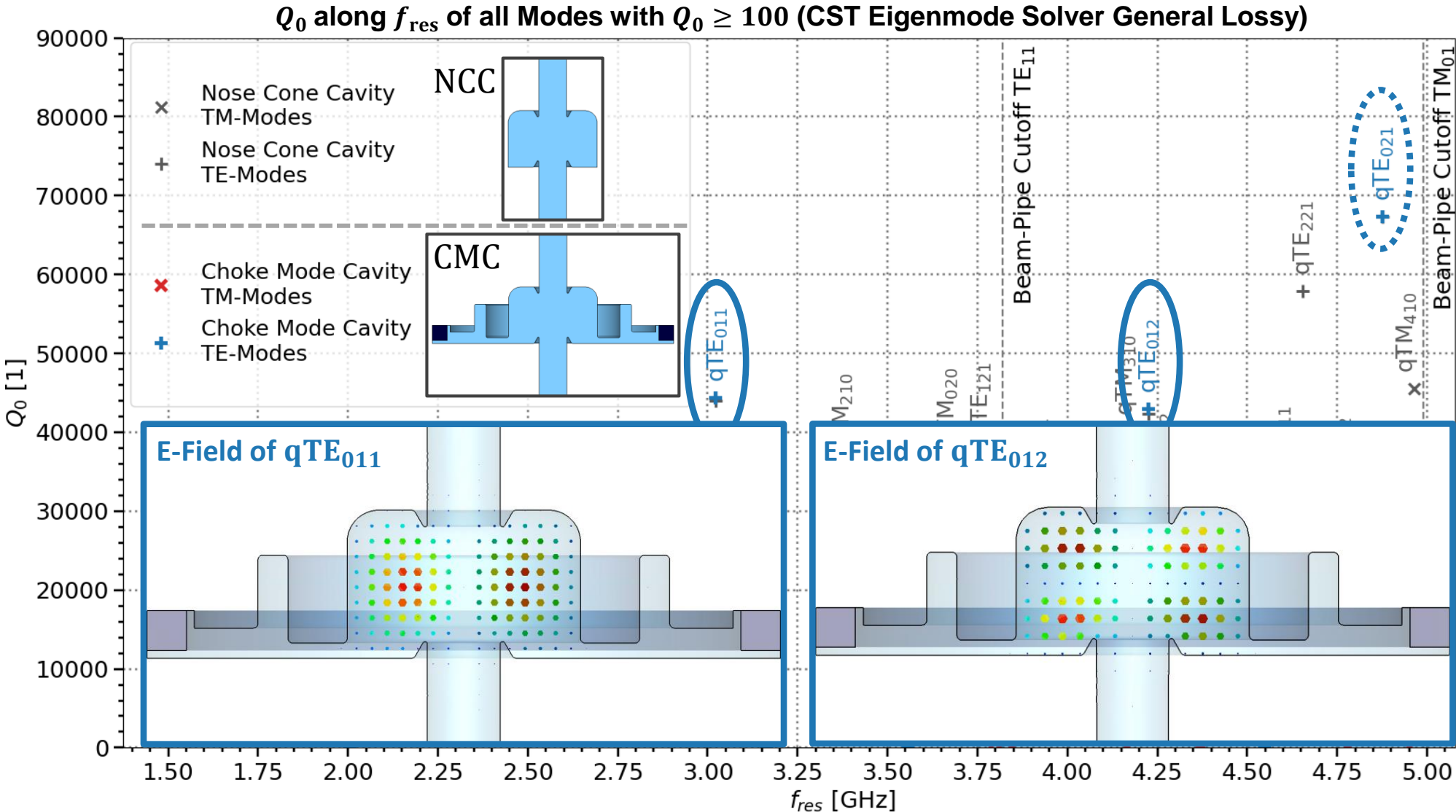
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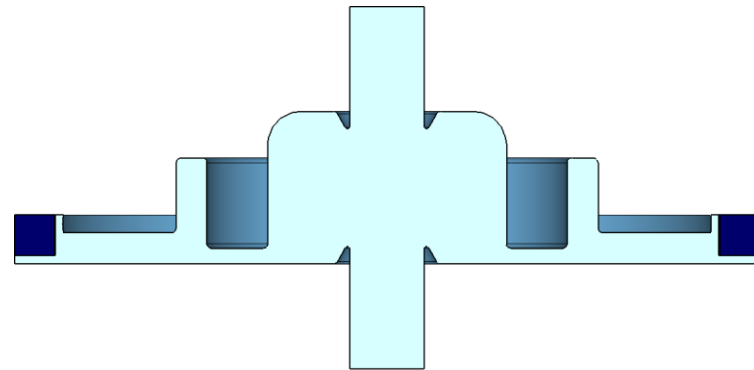


# 3. Coupler and Tuner System

## Specification of the Coupler & Tuner System

### Specification

- Keep manufacturing as simple as possible
  - Two Half Shells (Back & Top) without 45° Drilling
  - The Choke should not be turn around
- Actively adjustable Coupling Factor  
Range:  $K \approx 0.2$  to 5
- Broadband Tunable Resonant-Frequency  
Range:  $\Delta f_{\text{res}} \approx \pm 1.5$  MHz (or more)  
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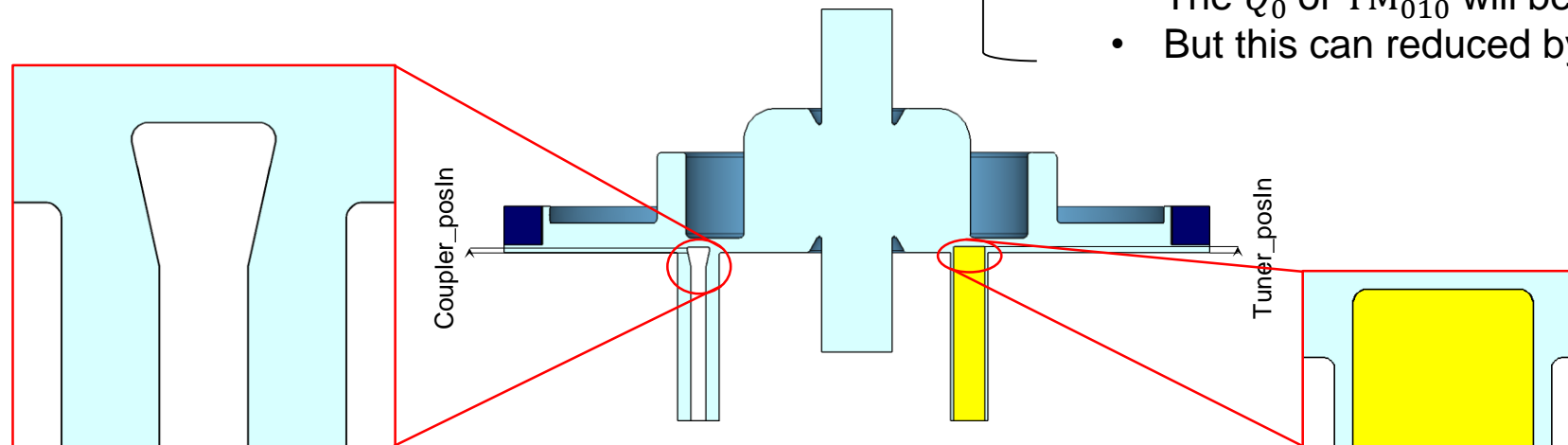
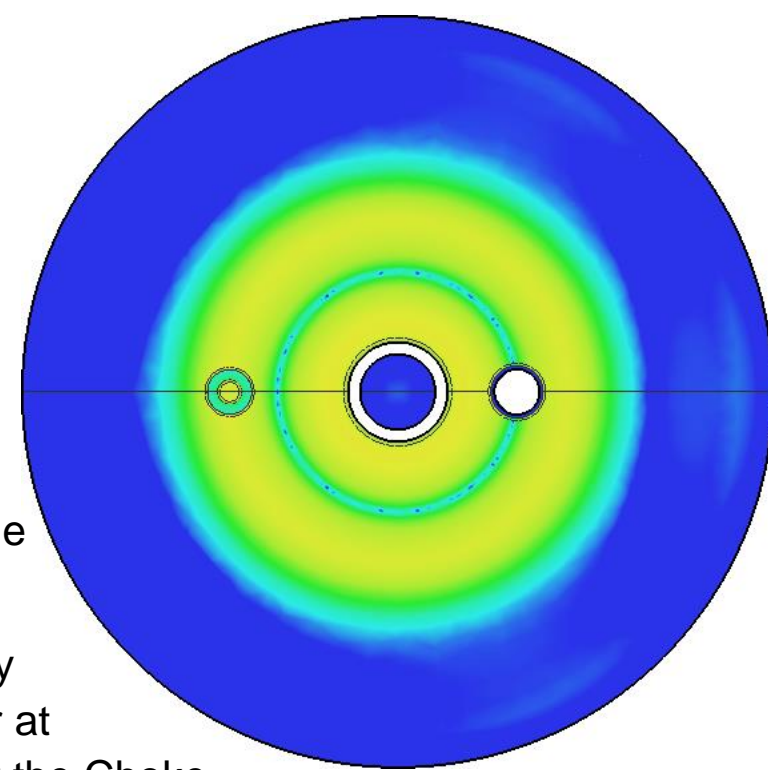
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### This is necessary:

- A capacitive Coupling and Tuning,
- Positioned in the Radial-Line

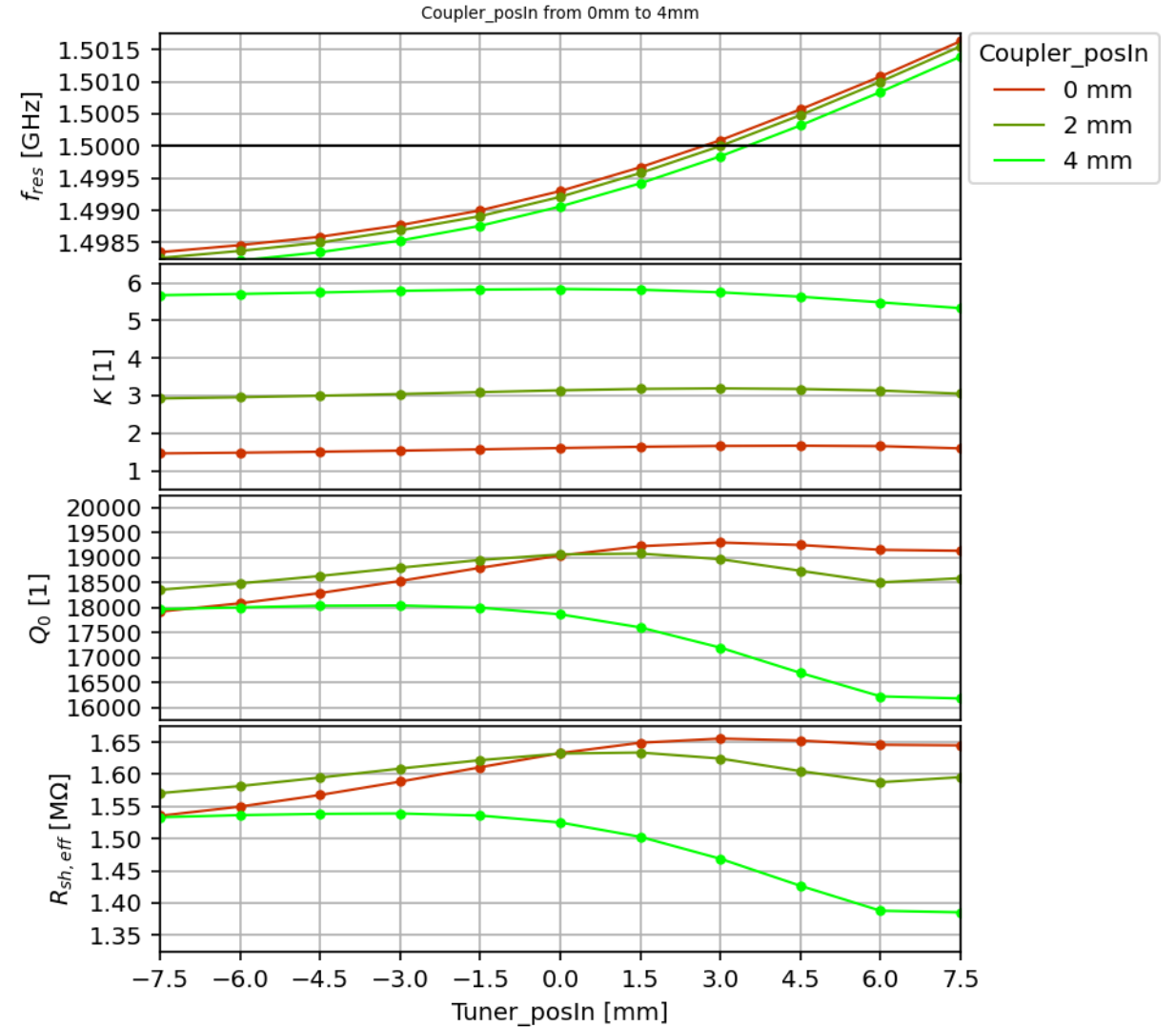
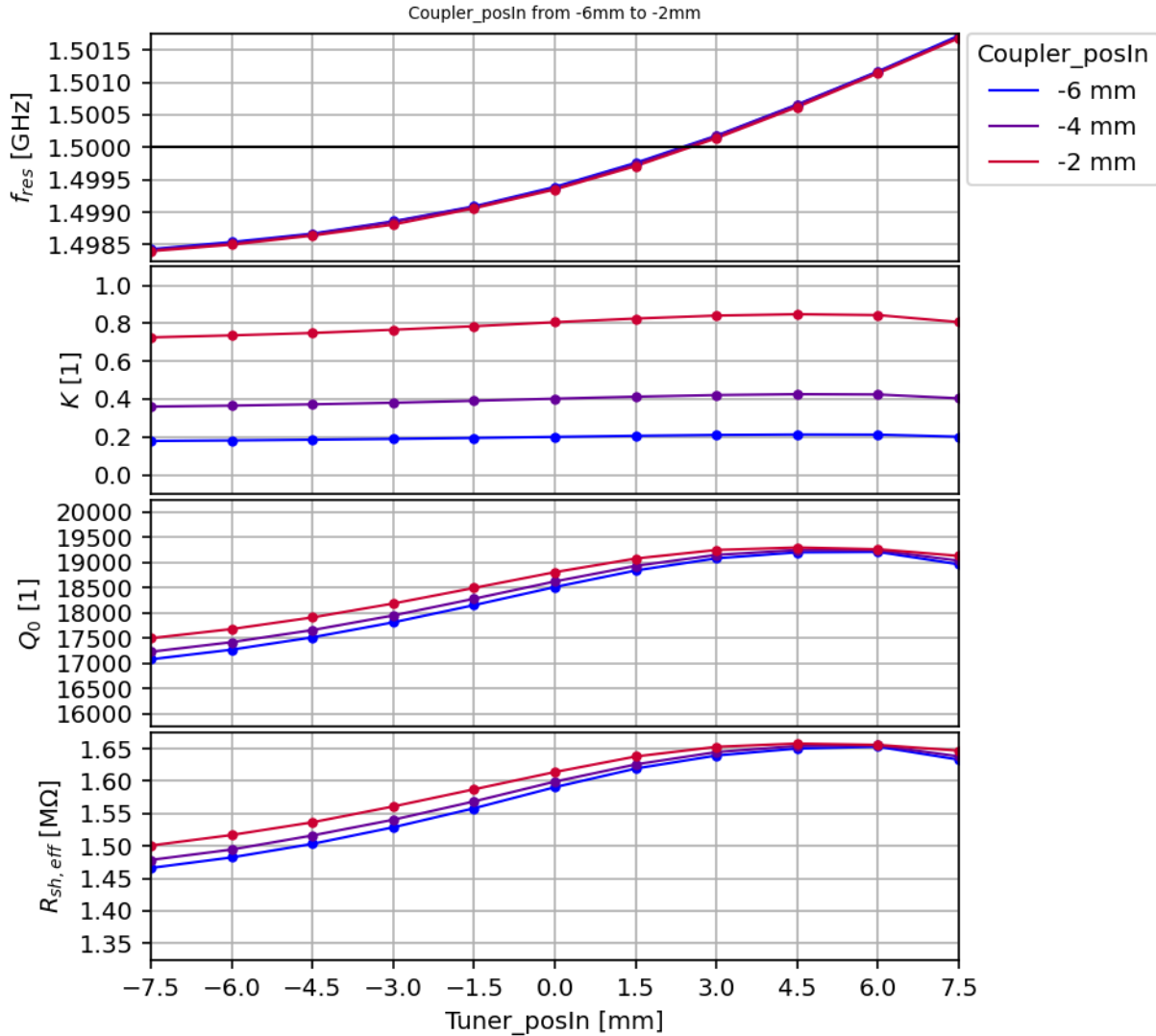
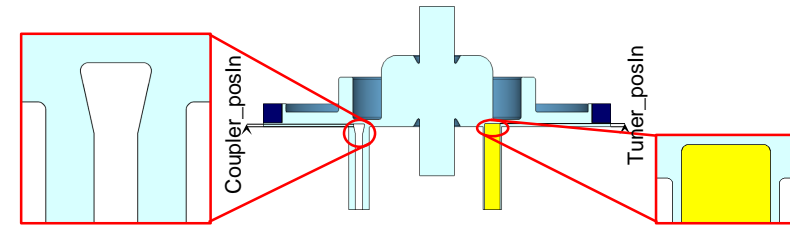
### Some Disadvantage:

- No longer perfect Symmetry
- Some part of the RF-Power at 1.5 GHz can tunneling throw the Choke
  - The  $Q_0$  of  $TM_{010}$  will be decreased in some way
  - But this can reduced by optimization



# 3. Coupler and Tuner System

## Coupler & Tuner in the Radial-Line



# Summary and Outlook

## Results & Next Steps

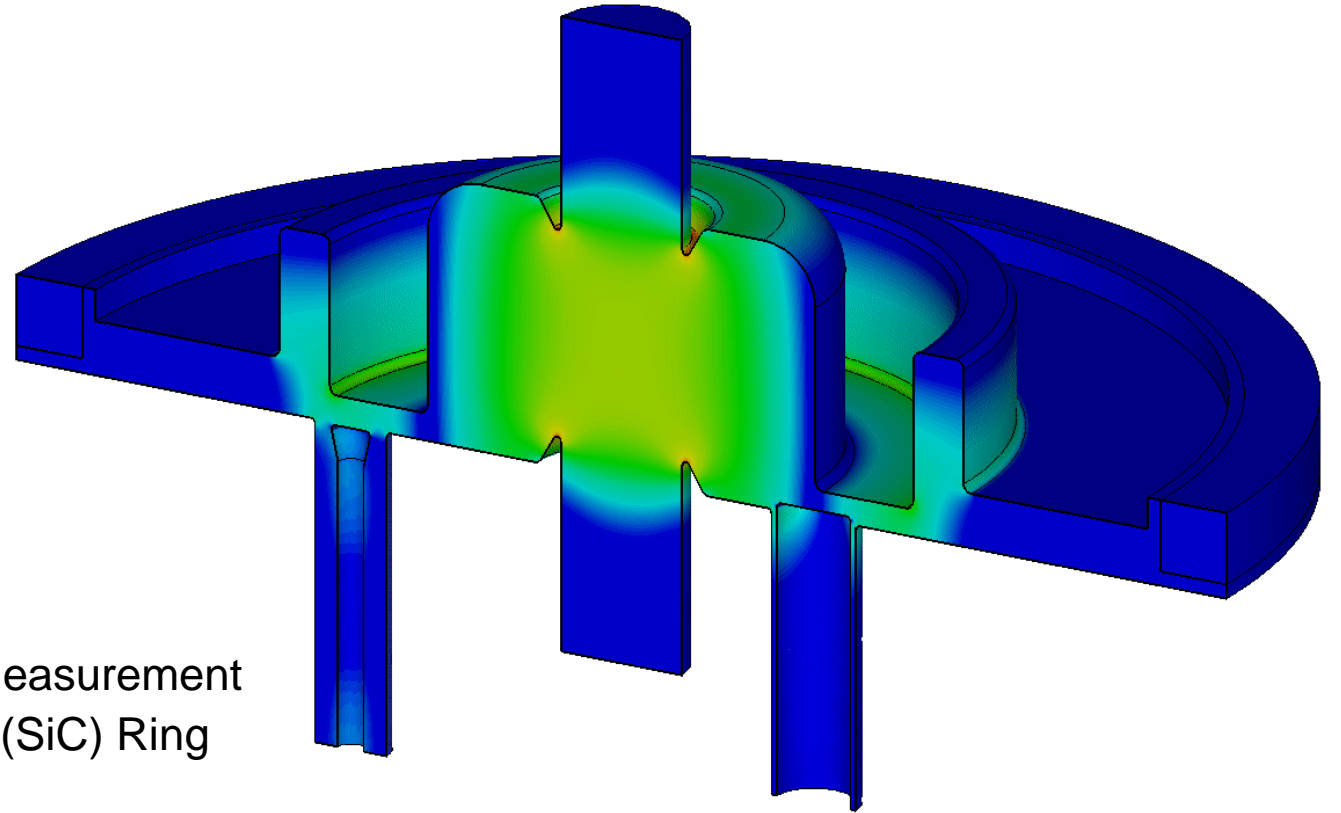
### Current Design

Simulated One-Cell 1.5 GHz Cavity Design

- Damping of all HOMs (Except  $TE_{0nq}$ )
- Coupling and Tuning in the Radial-Line
  - Adjustable Coupling-Factor
  - Broadband Tunable Resonant-Frequency
- With a very simple structure

### Next Steps

- Adding of Coaxial-Lines Sensors for Mode Measurement
- Selection and Purchase of an Siliconcarbid (SiC) Ring
- Creation of a Prototype



# Thank you

## References

1. T. Shintake, “The Choke Mode Cavity”, *Jpn. J. Appl. Phys.*, pp. pp. L 1567-L1570, 1992.
2. T. Inagaki et al., “High-gradient C-Band Linac for a Compact X-Ray Free-Electron Laser Facility”, *Phys. Rev. ST Accel. Beams*, vol. 17, p. 080702, 2014.

## Contact

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